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(72) Inventor: Orii, Shin
Kawaguchi-shi, Saitama-ken (JP)

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(74) Representative: Denmark, James
Bailey, Walsh & Co.
5 York Place
Leeds LS1 2SD Yorkshire (GB)

(71) Applicant: AHRESTY CORPORATION
Tokyo (JP)

(54) A Method of manufacturing metallic slurry for casting

(57) By putting molten metal in contact with a cooling unit, at least a portion of the molten metal is made

to rapidly cool into a semi-solid state and the molten metal is made to be held within a semi-molten temperature zone for a given time.

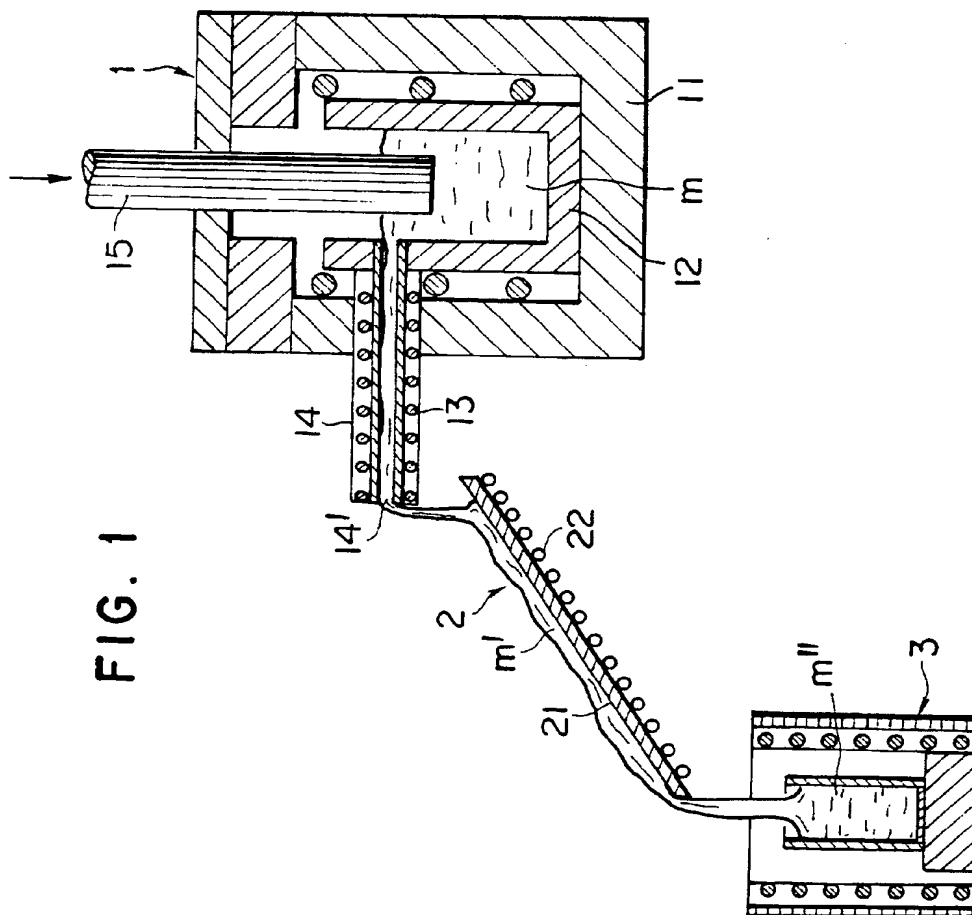


FIG. 1

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Description

Field of the Invention and Related Art Statement

This invention relates to a method of manufacturing metallic slurry for casting. More precisely, it relates to a method of manufacturing metallic slurry for casting, including metallic slurry for Rheocasting and metallic slurry for casting billets for Thixocasting, which is semi-solidified metallic slurry in which metal in a molten state (liquid phase) and metal in a solid state (solid phase) coexist and fine grains are mixed with liquid.

This kind of metallic slurry needs to be maintained in a state in which primary grains are separated from each other (by liquid matrix), and their crystal grains must be fine, homogeneous and non-dendritic, desirably globular. Slurry itself in such a state, or billet made by continuous casting and rapid cooling of the slurry and reheated becomes semi-molten metal of a high fraction solid and low viscosity, which can restrain shrinkage porosities in a casting and also improve its mechanical properties.

Various attempts have been offered for this reason.

A technique close to this invention was published in Japanese Patent Laid-Open No. Sho61-235047.

In the conventional technique, molten metal was poured on a temperature-controlled, inclined plate to produce a semi-molten metallic slurry as it flowed down the plate. However, the crystal grains became roseaceous and could not be satisfactorily globularized.

Object and Summary of the Invention

The object of this invention is to obtain metallic slurry for casting, particularly of aluminum alloys, and to offer a method of manufacturing such slurry by which fine, homogeneous non-dendritic (globular) crystal grains can be obtained by means of simple facilities without requiring a complex process.

The method invented to achieve such an object is characterized by an arrangement to rapidly cool at least a portion of molten metal consisting of an aluminum alloy into a semi-solid state by putting the molten metal in contact with a cooling unit, and hold the molten metal within a semi-molten temperature zone for a given time. It is also characterized desirably by the adjustment of the temperature of the molten metal contacting the cooling unit between liquidus temperature T_L and $T_L + 60^\circ \text{C}$, and also by the setting of the temperature of the molten metal at least a portion of which has been rapidly cooled into a semi-solid state between $(T_L - T_S)/2 + T_S$ (T_S represents solidus temperature) and $T_L + 40^\circ \text{C}$.

Further, it is characterized by an arrangement to make at least a portion of the molten metal contact a cooling unit by pouring and letting the molten flow on the cooling unit, which specifically is an inclined passage on which molten metal is poured and let to flow down, and the inclined passage is made in the shape of a plate, or

gutter, or pipe.

Brief Description of the Drawings

Figure 1 is a schematic diagram showing an example of embodiment of this invention.

Figure 2 is a microscopic picture of the structure of molten metal m' of which a portion has been quenched into a semi-solid state relating to an example of embodiment of this invention.

Figure 3 is a microscopic picture of the structure of metallic slurry relating to an example of embodiment of this invention.

Figure 4 is a microscopic picture of a billet made from metallic slurry related to an example of embodiment of this invention.

Figure 5 is a microscopic picture of the structure of molten metal a portion of which was quenched into a semi-solid state for comparison purpose.

Figure 6 is a microscopic picture of the structure of metallic slurry for comparison purpose.

Detailed Description of Preferred Embodiments

The method of manufacturing metallic slurry for casting which relates to this invention is described below with reference to the (schematic) shown in Figure 1. This invention, however, is not limited to (such an embodiment).

In the figure, numbers 1, 2 and 3 denote molten metal discharge furnace, cooling unit, and holding furnace, respectively.

The molten metal discharge furnace 1 is a furnace for accommodating and holding molten metal m of an aluminum alloy at a given temperature, or preferably at a temperature near the liquidus temperature, and it is composed of a well-known electric furnace 11 with a graphite crucible 12 inside, and a discharge feed pipe 14 equipped with a heater 13 and connected to the side thereof. Number 15 is a control rod to regulate the amount of discharged metal.

The cooling unit 2 is for rapidly cooling a portion of the molten metal m poured from the molten metal discharge furnace 1 into a semi-solid state by contact with the molten metal. It is made of a material, such as copper plate coated with solution resistant material, in the shape of a flat and smooth plate, or a gutter (split cylinder), or a pipe (cylinder), located directly under the feed hole 14' of the discharge feed pipe 14 in a sloping position to allow molten metal m to flow down, and providing an inclined passage 21 on its surface where molten metal m is poured to flow.

Number 22 in the figure is a cooling pipe to circulate a coolant, such as water, to control and maintain the surface of the cooling unit 2 at a given temperature.

The surface temperature of the cooling unit 2, or the inclined passage 21, is controlled depending on the pouring temperature and flow rate, etc. of molten m to

prevent it from flowing to the holding furnace 3 without creating a semi-solid state, or otherwise to prevent it from stagnating as it freezes.

Specifically, the temperature of molten metal m' before being held in the holding furnace 3, or molten metal m' at least a portion of which has been rapidly cooled into a semi-solid state by contacting the cooling unit 2, is controlled with the cooling unit 2 between $(T_L - T_S)/2 + T_S$ (T_S denotes solidus temperature) and $T_L + 40^\circ\text{C}$. In this connection, if the temperature of molten metal is lower than $(T_L - T_S)/2 + T_S$, the molten metal portion of which has been rapidly cooled into a semi-solid state ceases to flow on the cooling unit 2. If it becomes higher than $T_L + 40^\circ\text{C}$, the structure of metal m' held in the holding furnace 3 ends up as an undesirable structure which has grown dendritically.

By controlling the temperature of molten metal m' rapidly cooled by contact with the cooling unit 2 between $(T_L - T_S)/2 + T_S$ and $T_L + 40^\circ\text{C}$, the structure of the molten metal m' when plunged into ice water (or the like) and quenched becomes a very fine, granular structure even at liquids $T_L + \alpha$ (α below 40°C), whereas it was confirmed in an experiment that at the same (liquidus + α) the structure of molten metal not contacting the cooling unit 2 does not become granular, but fine, dendritic when plunged into ice water or the like and quenched at the same liquidus $T_L + \alpha$.

In this invention, the temperature of molten metal m at the same time it contacts the inclined passage 21 of the cooling unit 2 is adjusted between liquidus T_L and $T_L + 60^\circ\text{C}$. When the temperature of molten metal m is below liquidus T_L , it is difficult to control the cooling unit 2 and prevent molten metal m' from ceasing to flow on the inclined passage 21 of the cooling unit 2. When it is above $T_L + 60^\circ\text{C}$, it is also difficult to keep the semi-solid state of a portion of molten metal m' which has been put into contact with the surface of the inclined passage 21 of the cooling unit 2.

The holding furnace 3 is for getting the primary grains to grow and stabilizing the globularized state of molten metal m' at least a portion of which is in a semi-solid state, or has crystallized primary grains, by holding the molten metal m' at solid-liquid coexisting temperature for a given time.

For instance, a well-known electric furnace is used for the holding furnace 3.

When molten metal m in the molten metal discharge furnace 1 is poured through the discharge feed pipe 12 and let to flow down the inclined passage 21 of the cooling unit 2 after the molten metal temperature is adjusted between liquidus temperatures T_L and $T_L + 60^\circ\text{C}$, at least a portion of the molten metal m is rapidly cooled into a semi-solid state. And when the temperature of the molten metal m' rapidly cooled into a semi-solid state is controlled between $(T_L - T_S)/2 + T_S$ and $T_L + 40^\circ\text{C}$, by means of the cooling unit 2 and the molten metal is held in the holding furnace 3 within the semi-molten temperature zone ($T_S \sim T_L$) for a given time, good metallic

slurry m' with globular primary grains is obtained.

In an experiment, it was found that the holding time in the semi-molten metal temperature zone ($T_S \sim T_L$) in the holding furnace 3 is desirably 15 seconds or more; with an increase in the holding time, metallic slurry with more stabilized state of globularization was obtained.

[Embodiment]

Aluminum alloy AC4C of JIS was used for molten metal m, and the molten metal temperature at the time of contact with the surface of the inclined passage 21 of the cooling unit 2 and the temperature of molten metal m' a portion of which was rapidly cooled into a semi-solid state were set at 644°C (liquidus temperature + 30°C) and 634°C (liquidus temperature + 20°C) respectively. The obtained molten metal m' a portion of which had been rapidly cooled into a state of semi-solid state was plunged into ice water and quenched. A microscopic picture of the structure of the metal is shown in Figure 2.

In this microscopic picture, the white section is primary grains. If molten metal do not contact the cooling unit 2, the structure becomes fine-grained, but dendritic. It is observed that the molten-metal which contacted the cooling unit 2 formed a granular structure.

Then, by holding the molten metal m' a portion of which had been rapidly cooled into a semi-solid state in the holding furnace at 577°C for one minute, metallic slurry m" was obtained. A microscopic picture of the structure of the metallic slurry m" which was plunged into ice water and quenched is shown in Figure 3.

It is observed in this microscopic picture that the primary grains have grown in good, globular crystals. In the same picture, the white section was the primary grains (solid phase) when the metal was in slurry, and the black section was the molten portion when the metal was in slurry. This applies to the following microscopic pictures of metal structures.

For reference sake, a microscopic picture of the structure of a biller which was made by continuous casting of the metallic slurry m" is shown in Figure 4. It is observed in this picture that the primary grains consist of good, globular crystals.

[Comparison]

Metallic slurry m" was obtained by using the same molten metal as in the above-mentioned embodiment, and setting the temperature of molten metal at the time of contacting the surface of the inclined passage 21 of the cooling unit 2 at 684°C (liquidus temperature + 70°C) and the temperature of molten metal m' a portion of which had been rapidly cooled into a semi-solid state at 654°C (liquidus temperature + 40°C), and holding it in the holding furnace 3 at 577°C for one minute.

Figure 5 and 6 show microscopic pictures of the structures of the molten metal m' a portion of which had been rapidly cooled into a semi-solid state and the me-

tallic slurry m", which were both obtained under the above setting, and plunged into ice water and quenched as in the foregoing embodiment.

It can be seen from these microscopic pictures that primary grains have grown in dendritic crystals.

As described above, with the method relating to this invention of manufacturing metallic slurry for casting, fine-grained, nearly homogeneous non-dendritic (globular) primary grains can be obtained without the need of a complex process but with simple facilities.

Having described specific preferred embodiments of the invention with reference to the accompanying drawings, it will be appreciated that the present invention is not limited to those precise embodiments, and that various changes and modifications can be effected therein by one of ordinary skill in the art without departing from the scope and spirit of the invention as defined by the appended claims.

Also, it should be noted that although the specification is directed towards the creation of semi-molten metal slurries consisting of aluminium alloys, it is possible that other liquid alloys and elemental metal liquids may be used. In such cases the temperatures of the molten metal and of the cooling unit necessary to put the invention into practice are as proscribed in the specification for aluminium alloys.

Claims

1. A method of manufacturing metallic slurry for casting characterized by an arrangement to rapidly cool at least a portion of molten metal consisting of an aluminum alloy into a semi-solid state by putting the molten metal in contact with a cooling unit, and hold the molten metal within a semi-molten temperature zone for a given time.
2. A method of manufacturing metallic slurry for casting described in Claim (1) characterized by the adjustment of the temperature of the molten metal contacting the cooling unit between liquidus temperatures T_L and $T_L + 60^\circ \text{C}$.
3. A method of manufacturing metallic slurry for casting described in Claim (1) characterized by the setting of the temperature of the molten metal at least a portion of which has been rapidly cooled into a semi-solid state between $(T_L - T_S)/2 + T_S$ (T_S represents a solidus temperature) and $T_L + 40^\circ \text{C}$.
4. A method of manufacturing metallic slurry for casting described in Claim (1) characterized by an arrangement to make at least a portion of the molten metal contact the cooling unit by pouring and letting the molten metal flow on the cooling unit.
5. A method of manufacturing metallic slurry for casting described in Claim (4) characterized by the cooling unit being an inclined passage on which molten metal is poured and let to flow down.
6. A method of manufacturing metallic slurry for casting described in Claim (5) characterized by the inclined passage being made in the shape of a plate, or gutter, or pipe.

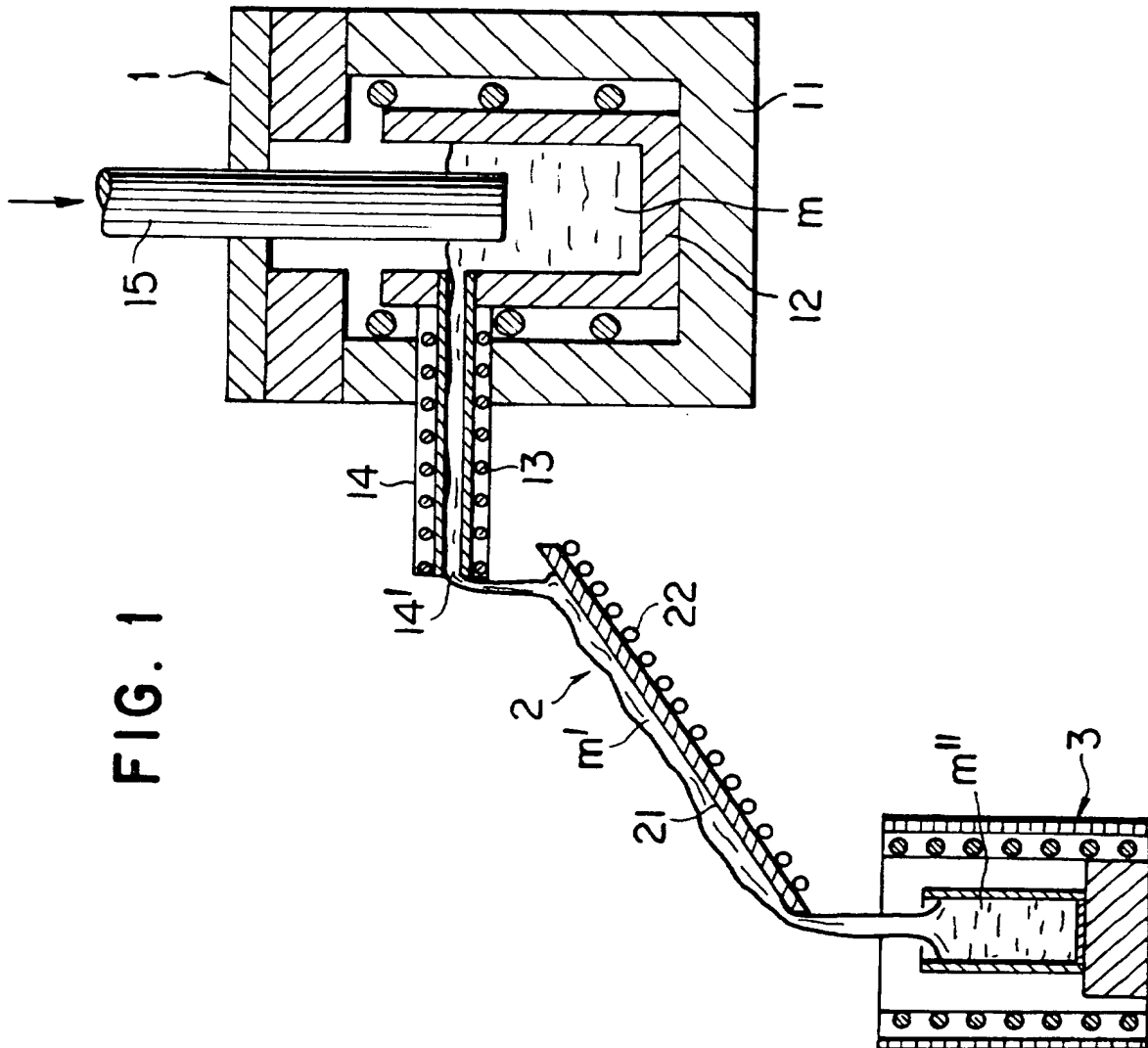


FIG. 2

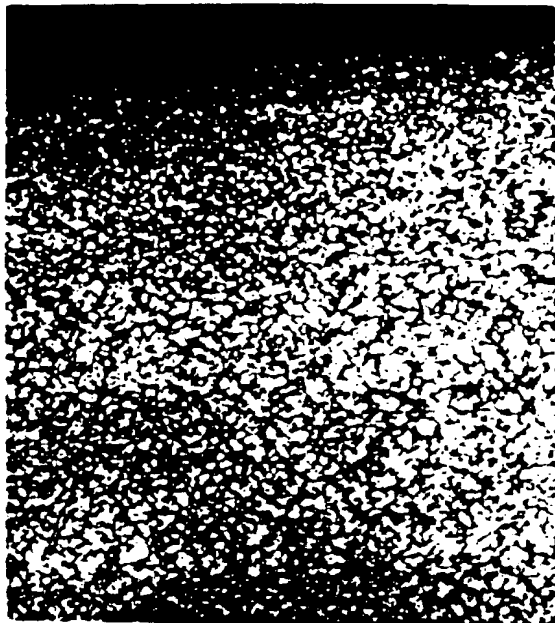


FIG. 3

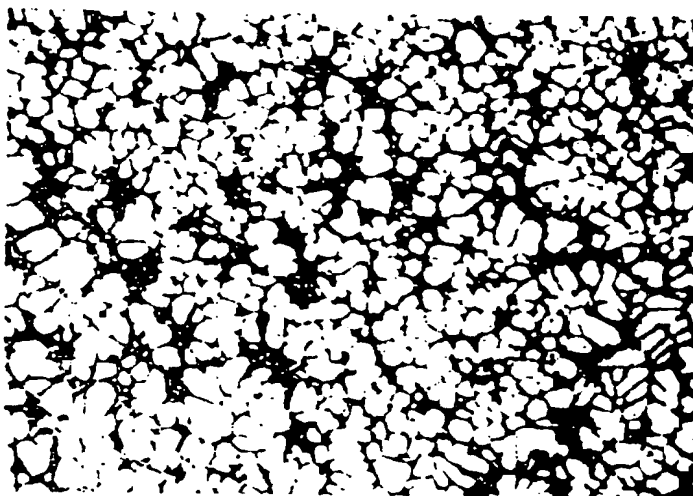


FIG. 4

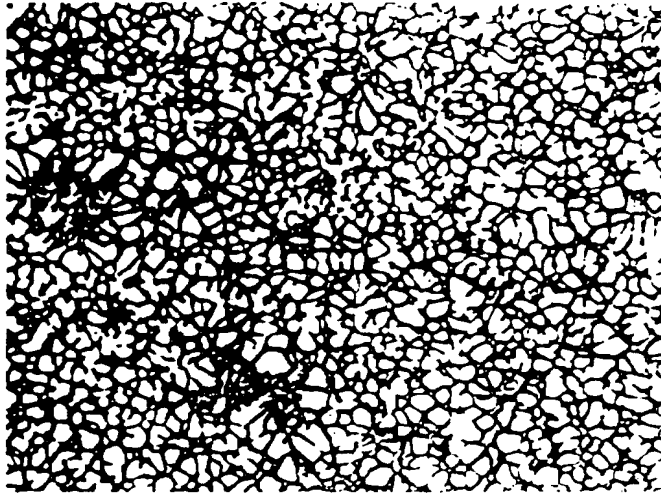
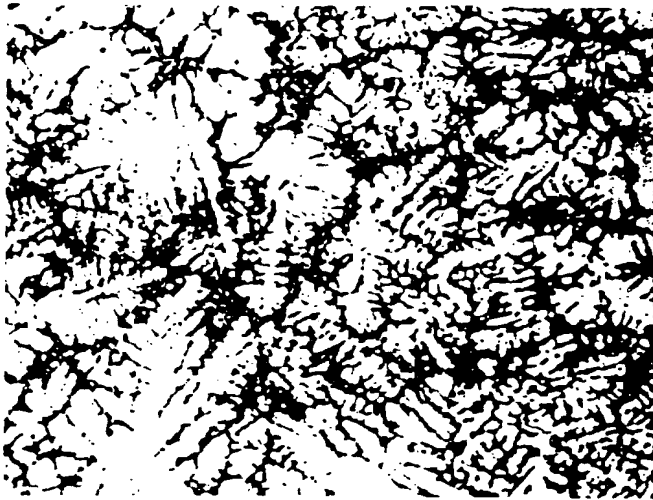


FIG. 5



FIG. 6





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EUROPEAN SEARCH REPORT

Application Number
EP 95 30 9498

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	EP-A-0 392 998 (CROSTI GIOVANNI ; POLVARA MARIA (IT)) 17 October 1990 * claims; figures 3,4 *	1-6	B22D1/00 C22C1/00
X	EP-A-0 089 196 (BRITISH STEEL CORP) 21 September 1983 * page 10, line 5 - line 20; figure 1 *	1-6	
X	EP-A-0 200 424 (NAT RES DEV) 5 November 1986 * claims; figures *	1-6	
X	EP-A-0 242 347 (CENTRE RECH METALLURGIQUE) 21 October 1987 * figures *	1-6	
A	GIESSEREI, vol. 81, no. 11, 6 June 1994, DUSSELDORF DE, pages 342-350, XP002000612 H. KAUFMANN: "Endabmessungsnahes Giessen: Ein Vergleich von Squeeze-casting und Thixocasting" * page 345, left-hand column, last paragraph - right-hand column, paragraph 1 *	1-6	TECHNICAL FIELDS SEARCHED (Int.Cl.6) B22D C22C
D,A	PATENT ABSTRACTS OF JAPAN vol. 011, no. 078 (M-570), 10 March 1987 & JP-A-61 235047 (NIPPON KOKAN KK), 20 October 1986, * abstract *	1-6	
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 16 April 1996	Examiner WOUDENBERG, S
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
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EPO FORM 1503 03/82 (P4/C8)